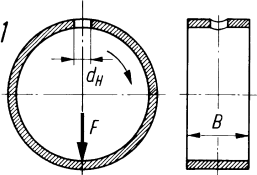
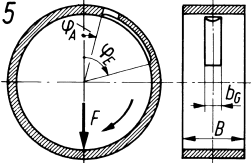
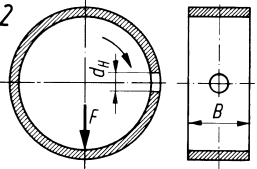
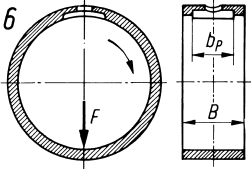
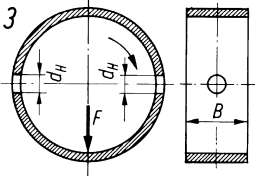
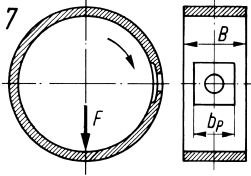
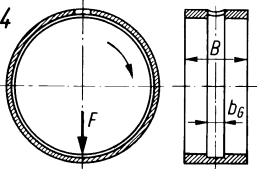
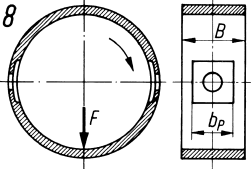


Tab. 17.19 Bezogenen Schmierdrehmoment  $q_2$  in Abhängigkeit von der Anordnung der Schmierstoff-Zuführungselemente (nach DIN 31652-2)

$q_2 = \frac{\pi}{48} \cdot \frac{(1 + \varepsilon)^3}{\ln \left( \frac{B}{d_H} \right)} \cdot q_H$ 	$q_2 \text{ siehe unten}$ 
$q_2 = \frac{\pi}{48} \cdot \frac{1}{\ln \left( \frac{B}{d_H} \right)} \cdot q_H$ 	$q_2 = \frac{\pi}{48} \cdot \frac{(1 + \varepsilon)^3}{\ln \left( \frac{B}{b_P} \right)} \cdot q_P$ 
$q_2 = \frac{\pi}{48} \cdot \frac{2}{\ln \left( \frac{B}{d_H} \right)} \cdot q_H$ 	$q_2 = \frac{\pi}{48} \cdot \frac{1}{\ln \left( \frac{B}{b_P} \right)} \cdot q_P$ 
$q_2 = \frac{\pi}{24} \cdot \frac{1 + 1,5 \cdot \varepsilon^2}{\left( \frac{B}{D} \right)} \cdot \frac{B - b_G}{B - b_G} \cdot q_H$ 	$q_2 = \frac{\pi}{48} \cdot \frac{2}{\ln \left( \frac{B}{b_P} \right)} \cdot q_P$ 
$q_2 = \frac{1}{48} \cdot \frac{\varphi_E - \varphi_A \cdot (1 + 1,5 \cdot \varepsilon^2) + (3 \cdot \varepsilon + \varepsilon^3) \cdot (\sin \varphi_E - \sin \varphi_A) + 0,75 \cdot \varepsilon^2 \cdot (\sin 2\varphi_E - \sin 2\varphi_A) - \frac{\varepsilon^3}{3} \cdot (\sin^3 \varphi_E - \sin^3 \varphi_A)}{\left( \frac{B - b_G}{D} \right)}$	
$q_H = 1,204 + 0,368 \cdot \left( \frac{d_H}{B} \right) - 1,046 \cdot \left( \frac{d_H}{B} \right)^2 + 1,942 \cdot \left( \frac{d_H}{B} \right)^3$	
$q_P = 1,188 + 1,582 \cdot \left( \frac{b_P}{B} \right) - 2,585 \cdot \left( \frac{b_P}{B} \right)^2 + 5,563 \cdot \left( \frac{b_P}{B} \right)^3 \quad \text{gültig für } 0,05 \leq \left( \frac{b_P}{B} \right) \leq 0,7$	